



Aspects of ISMAR performance

- How can we assess performance?
 - Basic sanity checks
 - Laboratory tests
 - Comparison with RT models
- What factors influence performance?
 - Thermal stability of receivers
 - Calibration target behaviour
 - Receiver linearity
 - Random noise



Receiver design









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Receiver thermal stability

- Gain of RF amplifiers is strongly dependent on temperature
 - Need to maintain stable temperature between scene and calibration views
 - Need to ensure output voltages remain in range of digitiser



• Frequency of Local Oscillators can be affected by temperature drifts

664-H



Receivers in flight





Impact of Rx temperature control

- During STICCS 664-H channel was particularly susceptible to voltage saturation due to lack of temperature control
- Improvements prior to COSMICS (low-temperature cutout on front-end cooling fan, extra insulation in IF enclosure) improved temperature stability and allowed voltages to mostly remain within digitizer range
- Power management issues during COSMICS meant optimum temperatures could not always be used (also an issue for hot calibration target)



Receiver voltage instability

 243-V initially noisy during STICCS – cabling issue resolved during campaign

 325 GHz receiver has ongoing issues with instability and noise





Calibration system

 Voltage measured during scene view converted to brightness temperature using

 $T_s = V_s \cdot G + O$

• Gain and offset calculated from frequent views of calibration targets:

$$G = \frac{T_h - T_c}{V_h - V_c} \qquad O = \frac{V_h T_c - V_c T_h}{V_h - V_c}$$

(in reality power is used)

• Errors in calibration target temperatures lead to errors in scene brightness temperatures:

$$\epsilon_{Tb_{scene}} = K\epsilon_{Tb_{hot}} + (1 - K)\epsilon_{Tb_{cold}}$$

$$K = \frac{V_{scene} - V_{cold}}{V_{hot} - V_{cold}} = \frac{Tb_{scene} - Tb_{cold}}{Tb_{hot} - Tb_{cold}}$$

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Calibration targets $\epsilon_{Theore} = K \epsilon_{Theor} + (1 - K) \epsilon_{Theore}$

$$K = \frac{V_{scene} - V_{cold}}{V_{hot} - V_{cold}} = \frac{Tb_{scene} - Tb_{cold}}{Tb_{hot} - Tb_{cold}}$$

- To minimise errors in scene temperature:
 - Small errors in power received when viewing target (i.e. target brightness temperature)
 - Accurate knowledge of target temperature across beam footprint
 - Target emissivity very close to 1
 - Large target temperature separation



Target temperature calculation

- Each target contains a number of PRTs for temperature measurement. Original processing used "closest" PRT for each channel. Update interpolates PRTs to channel positions and averages across beam footprints. All STICCS and COSMICS data now processed with update
- PRTs only provide coarse spatial sampling want to minimise thermal gradients across target





Hot target temperatures

- Want heated target as hot as possible with uniform temperature
- Initial flight trials showed that hot target struggled to maintain temperature due to airflow
- PP film installed prior to STICCS failed during first flight and deteriorated throughout campaign





Hot target temperatures

- Repaired film for COSMICS, care taken to ensure no sharp edges – much improved hot target stability and lasted for duration of campaign
- BUT requirement to manage heater power conservatively meant target was not always heated to optimum temperature





Cold target temperatures

- During STICCS, interference from scan motor causes noise and offsets on cold target PRTs
- Software work-around implemented during COSMICS pending improvements to hardware



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Target radiometric effects

- Is temperature measured by PRTs representative of the radiating parts of the target?
- Non-blackbody effects?



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Receiver linearity



Brightness temperature of LN2 cooled calibration target

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Receiver linearity - attenuation

 Attenuation reduces differences between 118GHz and 243GHz channels. Unable to test other channels as video amplifier re-tuning required



No additional attenuation was fitted during STICCS or COSMICS



B893 high altitude zenith views

- Aircraft flying just above tropopause
- Comparison with ARTS simulation using NWP model atmosphere. H₂O, O₂, N₂ and O₃ (climatology). H₂O and O₂ use PWR98 complete absorption models



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Receiver noise

- So far mostly considered biases. Random variation also important as it will affect ability to resolve cloud features
- Assuming *constant* Rx gain and offset:

$$\sigma_{V_s}^2 = \frac{1}{G^2} \frac{(T_s + T_{sys})^2}{B\tau}$$

• With single view of each calibration target:

$$\mathrm{NE}\Delta T^{2} = \frac{(T_{s} + T_{sys})^{2}}{B\tau} + \left(\frac{T_{s} - T_{h}}{T_{h} - T_{c}}\right)^{2} \frac{(T_{c} + T_{sys})^{2}}{B\tau} + \left(\frac{T_{s} - T_{c}}{T_{h} - T_{c}}\right)^{2} \frac{(T_{h} + T_{sys})^{2}}{B\tau}$$



Voltage deviations

- System noise temperatures as specified/measured during development (Y-factor test)
- Voltage deviations estimated using $\sigma_{V_h} \approx \sqrt{0.5\Delta V^2}$ to eliminate effects of long-term drifts

Channel	G (K/V)	T_{sys} (K)	<i>B</i> (GHz)	Calculated σ_{Vh}	Measured σ_{V_h}
118+1.1	63.2	700	0.4	0.003	0.003
118+1.5	67.2	700	0.4	0.002	0.003
118+2.1	72.5	700	0.8	0.002	0.002
118+3.0	71.3	700	1.0	0.001	0.002
118+5.0	68.9	700	2.0	0.001	0.001
243-H	64.4	1700	3.0	0.002	0.004
243-V	70.5	1850	3.0	0.002	0.002
325+1.5	83.3	2150	1.6	0.002	0.010
325+3.5	73.8	2100	2.4	0.002	0.007
325+9.5	73.3	2050	3.0	0.002	0.009
448+1.4	64.9	2500	1.2	0.004	0.008
448+3.0	71.1	3000	2.0	0.003	0.010
448+7.2	79.3	3500	3.0	0.003	0.015
664-H	69.5	2500	5.0	0.002	0.011
664-V	61.1	2000	5.0	0.002	0.021



NEDT

 Estimate NEDT from high altitude zenith views during B893 (assumes atmospheric variability small between successive views)

Channel	T_s (K)	T_h (K)	T_c (K)	T_{sys} (K)	B (GHz)	Calculated $NE\Delta T$	Measured $NE\Delta T$
118+1.1	78	325	276	700	0.4	1.0	0.5
118+1.5	51	325	276	700	0.4	1.1	0.5
118+2.1	35	325	276	700	0.8	0.9	0.4
118+3.0	22	325	276	700	1.0	0.8	0.7
118+5.0	17	325	276	700	2.0	0.6	0.4
243-H	5	325	276	1700	3.0	1.0	1.0
243-V	9	325	276	1850	3.0	1.1	0.6
325+1.5	9	325	276	2150	1.6	1.6	2.9
325+3.5	4	325	276	2100	2.4	1.3	1.4
325+9.5	6	325	276	2050	3.0	1.2	2.3
448+1.4	29	325	276	2500	1.2	2.0	2.1
448+3.0	14	325	276	3000	2.0	2.0	2.9
448+7.2	12	325	276	3500	3.0	1.9	5.1
664-H	15	326	276	2500	5.0	1.0	3.5
664-V	19	325	276	2000	5.0	0.8	7.0



Allan variance

• Standard variance estimate:

$$\frac{1}{N-1}\sum_{i=1}^N(y_i-\overline{y})^2$$

- does not converge with increasing N for non-white (i.e. time-correlated) noise
- Instead use difference between successive samples: $\frac{1}{2(M-1)} \sum_{i=1}^{M-1} [\bar{y}_{i+1} - \bar{y}_i]^2$
- Same as standard variance for white noise, but also converges for non-white noise
- Let yi be the mean of j successive samples. Plot Allan variance as a function of j



Allan variance examples





Allan deviation of Rx voltages



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Summary

- Overview of instrument performance during STICCS & ISMAR
- Improvements in thermal stability of receivers and calibration targets between the two campaigns
- Reasonable agreement with modelled zenith brightness
 temperatures at high altitude
- Calibration target temperature separation not always optimal during COSMICS due to power supply issue
- Issues with crosstalk, nonlinearity and possibly standing waves from calibration targets in some channels. Nonlinearity can be reduced with additional attenuation
- Excess noise on some receivers may be improved by increasing gain in IF chain



Questions?



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